

Study on the material and structural test program of stones with bonded anchors for performance-based design



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How reliably can the material properties of masonry structures be estimated from core samples?

BACKGROUND



Fig. 1 Examples of damage (Kumamoto earthquake)

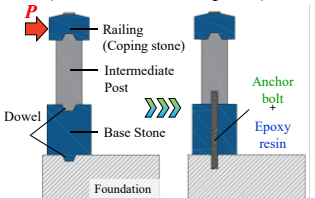


Fig. 2 Schematic illustration of bonded anchoring

Masonry structures (bridge, lantern, etc.) Condition

- Long-term use Deterioration
- Historic and aesthetic values Damage due to natural disasters
- Unique appearance

✓ Masonry structures should be strengthened while preserving their original appearance.
→ Bonded anchors can connect stones without changing their original appearances (Fig. 2).

Performance-based design

Design concept for verifying structural performance against required performance levels

Challenges

How many sampling cores are required to estimate each material properties?

Approach

Experimental evaluation of material properties using sampling cores.

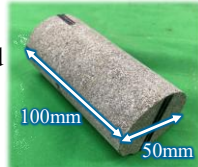


Fig. 3 A sampling core

METHOD

(1) Uniaxial compression test and measurement of nondestructive indicators

- ✓ Uniaxial compressive strength σ_c
- ✓ Young's modulus E
- ✓ Dry density ρ_d
- ✓ P-wave velocity V_p

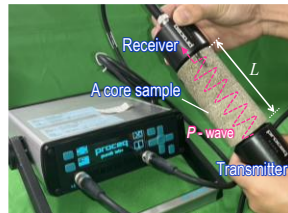


Fig. 4 Measurement of P-wave velocity

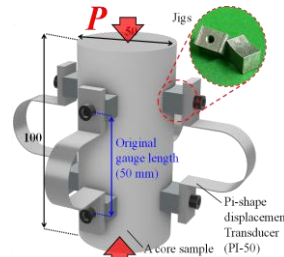


Fig. 5 Installation positions of measuring instruments

(2) Brazilian test

- ✓ Tensile strength σ_t

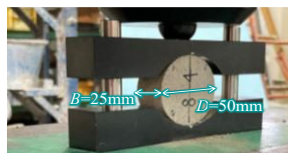


Fig. 6 Brazilian test

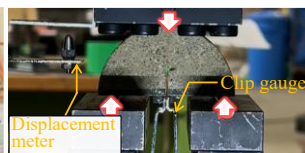


Fig. 7 SCB test

(3) SCB test

- ✓ Fracture toughness (Stress intensity factor K , Energy release rate G , Fracture energy G_F etc.)

RESULTS

- Database construction from core tests and literature survey
- Regression models using dry density ρ_d and P-wave velocity V_p
- Estimation of compressive strength σ_c and Young's modulus E

Multiple regression equations

$$E = \frac{1}{a} \rho_d^b \cdot V_p^c \quad (1) \quad \sigma_c = \frac{1}{d} \rho_d^e \cdot V_p^f \quad (2) \quad \sigma_c = gE \quad (3)$$

$$a (= 1,116.7 \text{ kg}^{0.533} \text{ MPa}^{-1} \text{ s}^{-1.571} \text{ m}^{-0.027}),$$

$$b (= 0.5328), c (= 1.5710),$$

$$d (= 0.6053), e (= 1.0810),$$

$$f (= 0.0213 \text{ kg}^{-1} \text{ MPa m}^3), g (= 0.0034)$$

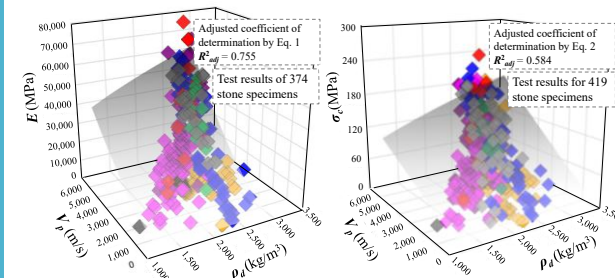


Fig. 8 $E - \rho_d - V_p$ relationship

Fig. 9 $\sigma_c - \rho_d - V_p$ relationship

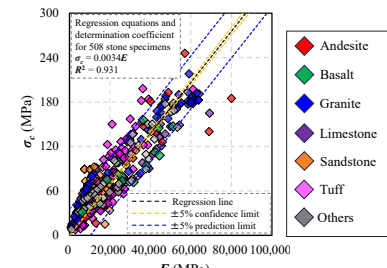


Fig. 10 $\sigma_c - E$ relationship

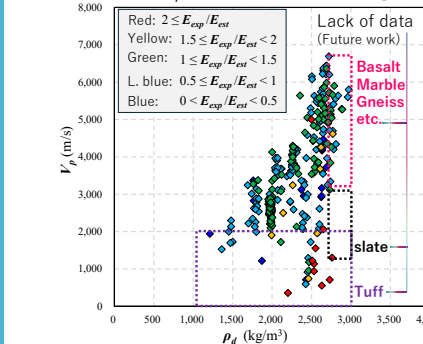


Fig. 11 Estimation error of Eq. (1) in $V_p - \rho_d$ plane

Discussion

- ✓ E and σ_c exhibited positive correlations with ρ_d and V_p .
- ✓ The estimation accuracy of σ_c was lower than E .
- ✓ The number of samples and estimation accuracy should be improved for tuff, slate, basalt, marble and so on

SUMMARY

- A material property database was constructed from sampling core tests and literature survey.
- Both E and σ_c showed positive correlations with ρ_d and V_p
- Noticeable deviations remained in σ_c estimation across stone types, indicating the need for further database expansion and additional parameters.

KEYWORDS

□ Masonry structures, material properties, Performance-based design